Thermal convection in inclined cylindrical containers

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By means of Direct Numerical Simulations (DNS) we investigate the effect of a tilt angle \(\beta\), \(0 \leq \beta \leq \pi/2\), of a Rayleigh–Bénard convection (RBC) cell of the aspect ratio 1, on the Nusselt number \(Nu\) and Reynolds number \(Re\). The considered Rayleigh numbers \(Ra\) are from \(10^6\) to \(10^8\) and Prandtl numbers are from 0.1 to 100 and the total number of the studied cases is 108. We show that the \(Nu(\beta)/Nu(0)\) dependence is not universal and is strongly influenced by a combination of \(Ra\) and \(Pr\). Thus, with a small inclination \(\beta\) of the RBC cell, the Nusselt number can decrease or increase, compared to that in the RBC case, for large and small \(Pr\), respectively. A slight cell tilting may not only stabilise the plane of the large-scale circulation (LSC) but can also enforce one for cases when the preferred state in the perfect RBC case is not an LSC but a more complicated multiple roll state. Close to \(\beta = \pi/2\), \(Nu\) and \(Re\) decrease with growing \(\beta\) in all considered cases. Generally, the \(Nu(\beta)/Nu(0)\) dependence is a complicated, non-monotonic function of \(\beta\).

Key words: Bénard convection, Convection in cavities, Turbulent convection

1. Introduction

Fluid motion driven by an imposed temperature gradient is a common phenomenon in nature and is important in many industrial applications. In the classical models of thermal convection, i.e. Rayleigh–Bénard convection (RBC) and vertical convection (VC), the fluid is confined between a heated and a cooled plate which are parallel to each other. The induced flow is determined by the Rayleigh number \(Ra \equiv \alpha g \Delta H^3/(\kappa \nu)\), Prandtl number \(Pr \equiv \nu/\kappa\) and the aspect ratio of the container \(\Gamma \equiv D/H\). Here \(\alpha\) denotes the isobaric thermal expansion coefficient, \(\nu\) the kinematic viscosity, \(\kappa\) the thermal diffusivity of the fluid, \(g\) the acceleration due to gravity, \(\Delta \equiv T_+ - T_-\) the temperature difference between the warm (\(T_+\)) and the cold (\(T_-\)) isothermal boundaries. We will only consider cylindrical vessels, characterised by the diameter \(D\) and the distance \(H\) between the heated and cooled plates.

The essential difference between RBC and VC is the direction of the gravity vector, i.e. it is parallel to the isothermal surfaces of the container in the case of VC and perpendicular to them in RBC. However, the respective flows are different and the Reynolds number \(Re\) and the mean heat flux, described by the Nusselt number \(Nu\), exhibit very different dependencies on \(Ra\) and \(Pr\). For reviews on these two classical convection models, we refer to Ahlers \textit{et al.} (2009); Bodenschatz \textit{et al.} (2000); Castaing

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et al. (1989); Chillà & Schumacher (2012); Lohse & Xia (2010); Siggia (1994) and to Ng et al. (2015), respectively.

Experimental studies of turbulent thermal convection in long cylinders filled with low-Prandtl-number fluids show that the convective heat transfer between the heated and cooled parallel surfaces of the container is most effective neither in a standing position of the cylinder (as in RBC, with a cell inclination angle $\beta = 0$), nor in a lying position (as in VC, $\beta = 0.5\pi$), but in an inclined container, for a certain intermediate value of $\beta$, $0 < \beta < 0.5\pi$. Such measurements in liquid sodium, $Pr \sim 0.01$, are reported by Frick et al. (2015); Kolesnichenko et al. (2015); Vasil’ev et al. (2015). Moreover, these experiments show that in the case of small $Pr$ ($Pr \ll 1$) and relatively large $Ra$ ($Ra \gtrsim 10^9$), any tilt $\beta$, $0 < \beta \leq \pi/2$, of the cell leads to an increase of $Nu$, compared to that in the RBC case ($\beta = 0$). Langebach & Haberstroh (2014) also obtained similar results in their experimental study for $Pr \approx 0.7$.

The effect of the cell tilting on convective heat transport in large-Prandtl-number fluids is very different from that in the case of low-Prandtl-number fluids. The following combinations of $\Gamma$, $Ra$ and $Pr$ were considered in our three-dimensional DNS: $Ra = 10^6$ for $Pr = 0.1, 1, 10$ and $100$; $Ra = 10^7$ for $Pr = 1$ and $10$; and $Ra = 10^8$ for $Pr = 1$. For each combination of $Ra$ and $Pr$ we studied thermal convection under the

2. Results

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Oberbeck–Boussinesq approximation, in inclined cylindrical containers with $\Gamma = 1$ and with different inclination angles $\beta$ that varied between 0 (RBC) and $\pi/2$ (VC). Thus, the problem is governed by the Navier–Stokes equations in cylindrical coordinates $(r, \phi, z)$:

$$\nabla \cdot \mathbf{u} = 0,$$

$$\frac{D_t}{\nu} \nabla^2 \mathbf{u} - \nabla p + \alpha g (T - T_0) \hat{e},$$

$$\frac{D_t}{\kappa} T = \nabla^2 T,$$

where $D_t$ denotes the substantial derivative, $\mathbf{u} = (u_r, u_\phi, u_z)$ the velocity vector, $p$ the reduced kinetic pressure, $T$ the temperature, $T_0 = (T_+ + T_-)/2$ and $\hat{e} = (-\sin(\beta) \cos(\phi), \sin(\beta) \sin(\phi), \cos(\beta))$. These equations are non-dimensionalized by using the cylinder radius $R$ and the quantities $(\alpha g R \Delta)^{1/2}, R(\alpha g R \Delta)^{-1/2}$ and $\Delta$ as units of length, velocity, time and temperature, respectively. (Note that in the definition of $Ra$, not the cylinder radius $R$, but the cylinder height $H$ is used as reference length.)

The resulting dimensionless equations are solved numerically with the code GOLDFISH, as in Shishkina & Wagner (2016); Shishkina et al. (2015). The computational grids of up to $(N_r, N_\phi, N_z) = (192, 512, 384)$ nodes satisfy the resolution requirements for DNS (Shishkina et al. 2010).
Olga Shishkina and Susanne Horn

Pr = 100 Pr = 10 Pr = 1 Pr = 0


\[ T^+ - T^- + T = 0 \] (RBC)

\[ \beta = 0 \]

\[ \pi \beta = 0 \]

\[ 0.05 \pi \]

\[ 0.1 \pi \]

\[ 0.15 \pi \]

\[ 0.2 \pi \]

\[ 0.25 \pi \]

\[ 0.3 \pi \]

\[ 0.35 \pi \]

\[ 0.4 \pi \]

\[ 0.45 \pi \]

\[ 0.5 \pi \]

Figure 2. Isosurfaces of the instantaneous temperature fields in inclined convection in cylindrical containers, filled with a fluid of \( Pr = 0.1, Pr = 1, Pr = 10 \) or \( Pr = 100 \), for \( Ra = 10^6 \) and different inclination angles from \( \beta = 0 \) to \( \beta = 0.5\pi \), as obtained in our DNS. Shown are ten isosurfaces that are equidistantly distributed between the heated \( (T^+) \) and cooled \( (T^-) \) cell boundaries.

The stepping in the \( \beta \)-range varies from \( 0.0025\pi \) to \( 0.05\pi \), with minimum 11 and maximum 22 different inclination angles between 0 (RBC) and \( \pi/2 \) (VC). The refined \( \beta \)-resolution is applied for cases that are near \( \beta = 0 \). This helps to better understand the behaviour of \( Nu \) and \( Re \) in inclined convection close to the exact RBC case, which is particularly relevant for experimental set-ups. In total we studied 108 different combinations of \( Ra, Pr \) and \( \beta \).

In figure 1 isosurfaces of the instantaneous temperature are presented for \( Pr = 1 \) and \( Ra = 10^6, 10^7 \) and \( 10^8 \), and 6 particular inclination angles \( \beta = 0 \) (RBC), 0.1\( \pi \), 0.2\( \pi \), 0.3\( \pi \), 0.4\( \pi \) and 0.5\( \pi \) (VC). In the RBC set-up \( (\beta = 0) \) the flows are always unsteady or even turbulent, and due to the aspect ratio of \( T = 1 \) and relatively small \( Pr \), the global flow
Thermal convection in inclined cylinders

For \( \beta = 0 \), the LSC is fixed to the inclination plane and likewise is its rotation direction. The flow is reorganised in such a way that fluid near the heated (cooled) plate ascends (descends) closer to the sidewall, hence most of the interior fluid is almost quiescent and has a mean temperature of about \( T = (T_+ + T_-)/2 \). For \( \beta \gtrsim 0.3\pi \) the interior temperature field shows signs of stratification, i.e. the temperature isosurfaces align horizontally. Further, with growing \( \beta \) the corner rolls are less pronounced (if exist) and the flow generally stabilizes. Thus, we observe steady flows for \( Ra = 10^6 \) if \( \beta \gtrsim 0.2\pi \), for \( Ra = 10^7 \) if \( \beta \gtrsim 0.3\pi \) and even for \( Ra = 10^8 \) if \( \beta \gtrsim 0.45\pi \). However, with increasing \( Ra \) and \( \beta = 0.5\pi \) (VC) the up-flow and down-flow along the isothermal plates becomes more vigorous and the impinging of the flow on the viscous boundary layer adjacent to the adiabatic wall leads to distinct overshoots in the temperature and will ultimately lead to a rolling up of the fluid and instability.

Furthermore, we conducted DNS for \( Pr = 0.1, 1, 10 \) and 100 for a fixed \( Ra = 10^6 \) (see figure 2) to investigate, how the cell tilt influences convection in fluids with different \( Pr \). For \( \beta = 0 \) the LSC develops in a single large-roll state if \( Pr \) is small, while for large \( Pr \) (\( Pr = 100 \)) a more complicated global flow structure develops (Horn et al. 2013; Horn & Shishkina 2014). With a tiny inclination angle \( \beta \) the flow is reorganized in a one-roll LSC even if \( Pr \) is large. Thus, for \( Pr = 100 \), we observe this already for \( \beta = 0.005\pi (= 0.9^\circ) \), see figure 3. Again, all flows are stabilized with growing \( \beta \). For \( Ra = 10^6, T = 1, \beta = 0 \) and all considered \( Pr \) the flows are unsteady, but already for \( \beta \gtrsim 0.06\pi \) (\( Pr = 100 \), \( \beta \gtrsim 0.15\pi \) (\( Pr = 10 \), \( \beta \gtrsim 0.2\pi \) (\( Pr = 1 \) and \( \beta \gtrsim 0.4\pi \) (\( Pr = 0.1 \) steady convective flows are observed.

Quantitative characteristics of the inclined convection flows, i.e. the Nusselt number,

\[
Nu(z) \equiv (\langle u_z T \rangle_z - \kappa \partial_z \langle T \rangle_z)/ (\kappa \Delta/H) = \text{const.},
\]

and the Reynolds number,

\[
Re \equiv \sqrt{\langle \mathbf{u} \cdot \mathbf{u} \rangle} H/\nu
\]

for different \( Pr \) are presented in figure 4. Here, \( \langle \cdot \rangle_z \) denotes the temporal and planar average at distance \( z \) from the heated plate and \( \langle \cdot \rangle \) denotes the average in time and over the whole convection cell.

The curves \( Nu(\beta) \) for small \( Pr \) (\( Pr = 1 \) and \( Pr = 0.1 \)) and large \( Pr \) (\( Pr = 10 \) and \( Pr = 100 \)) look very different (see figure 4a). In the small-\( Pr \) case \( Nu \) increases with any small tilt of a RBC (\( \beta = 0 \)) or VC (\( \beta = \pi/2 \)) cell. The global maximum of \( Nu \) is obtained for an intermediate value of \( \beta \). The absolute values of \( Nu \) are smaller for smaller
Pr (figure 4a), but the relative increase of the mean heat transport \( Nu(\beta)/Nu(0) \) is larger for smaller Pr (figure 4b).

The curves \( Nu(\beta) \) for large Pr (Pr = 10 and Pr = 100) almost replicate each other for \( \beta \geq 0.1\pi \) and differ only near \( \beta = 0 \). With a small tilt of the RBC cell (\( \beta \) close to 0) a tiny increase of \( Nu \) is possible. This effect is similar to that found by Weiss & Ahlers (2013) in their measurements in water. With further inclination of the cell, the \( Nu(\beta) \)-curve turns down; this drop of the Nusselt number is better pronounced for larger Pr. For \( Ra = 10^6 \) already by \( \beta \approx 0.05\pi \) the value of \( Nu(\beta) \) starts to grow till \( \beta \approx 0.4\pi \), where it reaches its global maximum and after that it decreases with growing \( \beta \) till \( \beta = \pi/2 \).

The Reynolds numbers are presented in the figures 4(c) and 4(d). On a log-scale the general behaviour of \( Re \) seems similar for all Pr, however, the normalised Reynolds numbers, \( Re(\beta)/Re(0) \), reveal a very different dependence on the cell tilt, especially for small \( \beta \). Remarkably, for Pr = 0.1 and 1 the Reynolds number increases while for Pr = 100 it decreases, and for Pr = 10, \( Re(\beta)/Re(0) \) drops, increases, and then drops again.

Both curves for Pr = 10 and for Pr = 100 show a couple of kinks which can be related to the different preferred large-scale flow states which can be steady or oscillatory. For Pr = 1 the initial increase with \( \beta \) is related to unsteady convection and a sufficiently efficient buoyancy-induced mixing of the bulk. For larger tilting angles \( 0.05\pi \lesssim \beta \lesssim 0.15\pi \) the flow stabilises, and an oscillating LSC develops that is reflected in the slow decrease in \( Re \). Finally, for completely steady convection at \( \beta \gtrsim 0.15 \), \( Re(\beta)/Re(0) \) decreases,
Thermal convection in inclined cylinders

but now much sharper. Similarly, for $Pr = 0.1$, the initial increase up to $\beta \approx 0.15\pi$ is due to the unsteady mixing in the bulk. The competing effect of stratification caused by the inclination then leads first to a gentle down-slope. Eventually, for $\beta \gtrsim 0.3\pi$, the flow becomes steady and $Re(\beta)/Re(0)$ drops abruptly. Hence, in all cases $Re(\beta)/Re(0)$ decreases with growing $\beta$ near $\beta = \pi/2$ (VC state) with similar slope. This decrease is only slightly steeper for larger $Pr$.

The Rayleigh number is besides $Pr$ evidently the other important control parameter that influences the $Nu$- and $Re$-dependencies on inclined thermal convection. Thus, we conducted DNS for $Pr = 1$ where we varied $Ra$ from $10^6$ to $10^8$, and DNS for $Pr = 10$ with $Ra = 10^6$ and $10^7$. The results are shown in figure 5.

As expected, for almost all considered $Ra$, $Nu(\beta)/Nu(0)$ grows near $\beta = 0$ and decreases near $\beta = \pi/2$, see figure 5(a)–(b). Otherwise, the curves do not show a very distinct or apparent regularity dependent on $Ra$. The principle structure of the $Nu(\beta)/Nu(0)$-profiles (figure 5(b)) is determined mainly by $Pr$. For $Pr = 1$, the function $Nu(\beta)/Nu(0)$ has one maximum for $Ra = 10^6$ and at least two maxima and one minimum for $Ra = 10^7$ and $Ra = 10^8$. The first maxima for $Ra = 10^7$ and $10^8$ are at about the same $\beta$. However, the heat transfer is most efficient at an inclination of $\beta = 0.25\pi$ for $Ra = 10^6$ and $Ra = 10^8$, but closer to the RBC case at $\beta = 0.1\pi$ for $Ra = 10^7$.

A $Pr = 10$ fluid behaves differently. In both studied cases, for $Ra = 10^6$ and $Ra = 10^7$, the heat transport is most efficient for $\beta = 0.4\pi$, i.e. closer to VC. For $Ra = 10^7$ there is
Olga Shishkina and Susanne Horn

\[(H/\nu)Pr^{1/2}Ra^{-1/2}u_\tau\]

\[(H^4/\nu^3)Pr^2Ra^{-1}(Nu - 1)^{-1}\epsilon_u\]

Figure 6. Normalized (a) friction velocity \(u_\tau\), averaged in time and over the top and bottom plates, and (b) time- and volume-averaged kinetic dissipation rate \(\epsilon_u\), in inclined convection in a cylinder of the aspect ratio 1, for \(Pr = 0.1\) (triangles), \(Pr = 1\) (squares), \(Pr = 10\) (circles) and \(Pr = 100\) (diamonds), and \(Ra = 10^6\) (open symbols), \(Ra = 10^7\) (half filled symbols) and \(Ra = 10^8\) (filled symbols), as functions of the inclination angle \(\beta\).

Another pronounced maximum at \(\beta = 0.05\), albeit lower in magnitude. Contrary to that, for \(Ra = 10^6\), the \(Nu(\beta)/Nu(0)\) curve has a minimum at the very same \(\beta\). For \(Ra = 10^6\) only an almost negligible heat flux intensification can be found for small tilt angles, at the tiny angle of \(\beta = 0.005\pi\).

For all Prandtl numbers considered, the Nusselt number in the VC case becomes gradually smaller relative to the RBC case, with increasing \(Ra\); and for \(Ra = 10^8\) and \(Pr = 1\) it is even below it. But neither VC nor RBC seem to be clearly distinguished states in terms of the heat transport.

The Reynolds number, on the other hand, shows at least for \(\beta \gtrsim 0.25\pi\) a much more regular dependence on \(\beta\), see figure 5(c)–(d). For all cases, the relative Reynolds number \(Re(\beta)/Re(0)\) was found to decrease near \(\beta = \pi/2\), and stronger for larger \(Ra\). Again, the largest variation of \(Re(\beta)/Re(0)\) is found near \(\beta = 0\): first it increases with \(\beta\) near \(\beta = 0\) and then, after its maximum which is achieved within the inclination interval \([0; 0.1\pi]\), it gradually decreases.

In an attempt to gain some further insight into the complicated \(Nu(\beta)\) and \(Re(\beta)\) behaviour, we studied the friction velocity \(u_\tau\) at the bottom plate, evaluated as

\[u_\tau^2 = \nu \partial_z \left( \langle u_r^2 + u_\phi^2 \rangle \right)_{z=0}^{1/2}\]

and presented in figure 6(a). Contrary to the naive assumption that it should be highest for VC, since in this case the core of the fluid is stably stratified and the flow along the boundaries is a developed shear flow, the friction velocity is maximal for \(\beta = 0.4\pi\). Indeed, the maximum shear velocity \(u_\tau\) coincides with the maximum of \(Nu\) for large \(Pr\). Very likely it also contributes to the intensification of \(Nu\) with decreasing \(\beta\) compared to the VC case for all \(Pr\). But it is not the only mechanism, and certainly not the dominant one for smaller \(Pr\) and higher \(Ra\). Here, the buoyancy-induced mixing and the more efficient transport by plumes along the cylinder sidewall, in particular for smaller \(\beta\), seems to predominantly determine the behaviour of \(Nu\) and \(Re\) with \(\beta\).

Finally, we evaluate the time- and volume-averaged kinetic dissipation rate \(\epsilon_u = \langle \nu \sum_i (\nabla u_i)^2 \rangle\). In the particular case of \(\beta = 0\) (RBC) the following exact relation holds:

\[\epsilon_u = (\nu^3/H^4)Pr^{-2}Ra(Nu - 1)\]

With growing but still small inclination angle \(\beta\), the normalised kinetic dissipation rate \((H^4/\nu^3)Pr^2Ra^{-1}(Nu - 1)^{-1}\epsilon_u\) might slightly increase,
Thermal convection in inclined cylinders

3. Discussion

The conducted DNS show that the Nusselt number and Reynolds number dependencies in inclined convection are generally non-monotonic complicated functions of $Ra$ and $Pr$. Obviously, the geometry of the convection cell also influences these dependencies. The results are summarised in figure 7, where phase diagrams for $Nu_{0}^{-1}$ and $Re_{0}^{-1}$ are presented in the $(Pr, \beta)$ plane. These diagrams show the regions of relative deviations of $Nu$ and $Re$ with respect to the RBC case ($\beta = 0$), as it was obtained in the DNS.

In contrast to RBC ($\beta = 0$), in VC ($\beta = \pi/2$) the turbulent processes are much weaker, but the LSC is more coherent. In both limiting cases the heat transport is generally not as effective as in inclined convection, as it was obtained in all cases studied here ($Ra \leq 10^8$).

For small-Prandtl-number fluids, the velocity of the LSC (reflected in $Re$) starts to increase with $\beta$ already for a tiny tilt of the RBC cell, which leads to a more effective heat transport. Thus, a felicitous combination of buoyancy and shear in IC in fluids with $Pr \ll 1$ can lead to a significant increase of the mean heat flux, as it was obtained by Frick et al. (2015); Kolesnichenko et al. (2015). The increase of $Nu$ compared to that in the RBC case is found to be larger for smaller $Pr$ and higher $Ra$.

Contrary to the small-$Pr$ fluid flows, for large $Pr$, a maximum of $Re(\beta)$ is obtained close to $\beta = 0$. The absolute increase of the LSC velocity due to the cell inclination is small, if any, and after a possible maximum the Reynolds number decreases gradually with increasing $\beta$. This drop of $Re$ is stronger for larger $Ra$. Thus, in large-$Pr$ fluids by high $Ra$, an increase of the heat transport due to an additional shear is not expected, and this is supported by a recent experiment by Guo et al. (2015), where a gradual decrease of $Nu$ with the cell inclination was obtained for $Pr \approx 6.7$ and $Ra \approx 4.4 \times 10^9$. We anticipate further, that for larger $Ra$ and $Pr > 1$, the decrease of $Nu(\beta)$ with increasing $\beta$ will be better pronounced by the following reasons. As our simulations show, for larger $\beta$, the onset of turbulence requires larger $Ra$. Therefore, for the same $Ra$ the flow can be already in the fully turbulent regime in the case $\beta = 0$ (RBC) and still in the laminar or transitional regime in the case $\beta = \pi/2$ (VC). Since the scaling exponents in the $Nu$-$vs.-Ra$ scaling are generally larger for the turbulent regimes (Grossmann & Lohse 2000;
Schlichting & Gersten 2000), the ratio of the Nusselt number at $\beta = \pi/2$ to the Nusselt number at $\beta = 0$ will gradually decrease with growing $Ra$ in that range. The behaviour of $Nu(\beta)$ in large-$Pr$ fluids near $\beta = 0$ is quite complicated. A non-monotonicity of $Nu(\beta)$ in that region cannot be explained exclusively by a single- or multiple-roll structure of LSC, as the non-monotonic dependencies were obtained also in the regions where a clear dominance of a single-roll global flow structure was observed.

The complicated behaviour of the $Nu$ vs. $Ra$ dependence, with multiple extrema, in the studied range of $Ra$ and $Pr$ can be explained by the interaction of different transitions. Thus, for a fixed parameter $\beta = 0$ (RBC), the flow can vary from a steady one for small $Ra$ to a turbulent one for large $Ra$. Even when two parameters are fixed, namely, the Rayleigh number at a certain moderate value and $\beta = 0$, the flow can be turbulent for small $Pr$ (Frick et al. 2015; Horn & Shishkina 2015; Shishkina et al. 2013, 2014) or non-turbulent (irregularly or periodically time dependent) for large $Pr$ (Krishnamurti 1970; Bosbach et al. 2012; Horn & Shishkina 2014; Horn et al. 2013). When also the parameter $\beta$ varies, the situation becomes even more complicated, as with growing $\beta$ the onset of turbulence moves to larger $Ra$. Moreover, with changing $\beta$, the flow symmetries change, which influence the $Nu(Ra, Pr, \beta)$ and $Re(Ra, Pr, \beta)$ dependences (see also Wei et al. (2015) on sharp transitions in RBC, caused by changes of flow symmetries).

For larger $Ra$, where the convection flows are turbulent for all $\beta$, the dependences should be simpler. As discussed, for large $Ra$ we expect a monotonic reduction of $Nu$ with growing $\beta$ for large $Pr$, as in the experiments by Guo et al. (2015), and a single maximum for an intermediate value of $\beta$ in the $Nu$ vs. $\beta$ dependence for the case of small $Pr$, as it was obtained in the measurements by Frick et al. (2015); Kolesnichenko et al. (2015); Langebach & Haberstroh (2014); Vasil’ev et al. (2015). Further investigations of inclined convection in different fluids, both, experimentally and numerically, for large and small $Pr$, are required for a better understanding of the IC driving mechanisms and its $Re(\beta)$- and $Nu(\beta)$-dependences.

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